

**WEST VIRGINIA**  
**SECRETARY OF STATE**  
**KEN HECHLER**  
**ADMINISTRATIVE LAW DIVISION**

Form #2

FILED  
1988 SEP 10 PM 4:25  
WEST VIRGINIA  
STATE SECRETARY OF STATE

**NOTICE OF A COMMENT PERIOD ON A PROPOSED RULE**

AGENCY: Air Pollution Control Commission TITLE NUMBER: 45

RULE TYPE: Legislative; CITE AUTHORITY Chapter 16-20

AMENDMENT TO AN EXISTING RULE: YES \_\_\_ NO X

IF YES, SERIES NUMBER OF RULE BEING AMENDED: \_\_\_\_\_

TITLE OF RULE BEING AMENDED: \_\_\_\_\_

IF NO, SERIES NUMBER OF NEW RULE BEING PROPOSED: TP-2

TITLE OF RULE BEING PROPOSED: "Compliance Test Procedures for Regulation II -  
To Prevent and Control Particulate Air Pollution From Combustion of Fuel  
in Indirect Heat Exchangers"

IN LIEU OF A PUBLIC HEARING, A COMMENT PERIOD HAS BEEN ESTABLISHED DURING WHICH ANY INTERESTED PERSON MAY SEND COMMENTS CONCERNING THESE PROPOSED RULES. THIS COMMENT PERIOD WILL END ON November 15, 1988 AT 4:45 p.m. ONLY WRITTEN COMMENTS WILL BE ACCEPTED AND ARE TO BE MAILED TO THE FOLLOWING ADDRESS.

Mr. Carl G. Beard, II

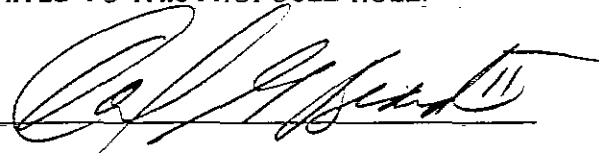
Director

WV Air Pollution Control Commission

1558 Washington Street, East

Charleston, WV 25317

THE ISSUES TO BE HEARD SHALL BE LIMITED TO THIS PROPOSED RULE.



ATTACH A **BRIEF** SUMMARY OF YOUR PROPOSAL

ABSTRACT

Regulation TP-2 (1988) was adopted by the Commission on the \_\_\_\_\_  
day of \_\_\_\_\_, \_\_\_\_\_ and became effective \_\_\_\_\_,  
\_\_\_\_\_, and was filed with the Secretary of State \_\_\_\_\_,  
\_\_\_\_\_.

WEST VIRGINIA ADMINISTRATIVE REGULATIONS

Subject: TP-2 - "Compliance Test Procedures for Regulation II - 'To Prevent and Control Particulate Air Pollution From Combustion of Fuel in Indirect Heat Exchangers'"

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WEST VIRGINIA ADMINISTRATIVE REGULATIONS  
Air Pollution Control Commission

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SEP 16 PM 4:25

Chapter 16-20  
Series TP-2  
(1988)

SECRETARY OF STATE

Subject: TP-2 - "Compliance Test Procedures for Regulation II - "To Prevent and Control Particulate Air Pollution From Combustion of Fuel in Indirect Heat Exchangers"

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**Section 1. General.**

1.1. Scope.

It is the intent of and purpose of this procedural rule to establish stack testing procedures for determination of compliance with the weight emission standards as set forth in the Commission's Regulation II - "To Prevent and Control Particulate Air Pollution From Combustion of Fuel in Indirect Heat Exchangers". To this end, it is the intent of the Commission to adopt by reference, certain of the Reference Methods and other test methods set forth in 40 CFR, Part 60, Appendix A [as of July 1, 1988]. These methods set forth acceptable stack testing, calibration, and laboratory procedures including appropriate apparatus with provisions for certain minor exceptions as delineated in Section 6 of this procedural rule.

1.2. Authority.

This rule is issued under the authority of the West Virginia Code, Chapter 16, Article 20, Section 5. This rule relates to West Virginia Code, Chapter 16, Article 20, Sections 1 through 13 inclusive.

1.3. Filing Date.

This rule was adopted by the Commission on the \_\_\_\_\_ day of \_\_\_\_\_, 1988, and filed with the Secretary of State on the \_\_\_\_\_ day of \_\_\_\_\_, 1988.

1.4. Effective Date.

This rule shall become effective on the \_\_\_\_\_ day of \_\_\_\_\_, 1988.

**Section 2. Definitions.**

2.1. "Commission" shall mean the West Virginia Air Pollution Control Commission.

2.2. "Director" shall mean the Director of the West Virginia Air Pollution Control Commission.

2.3. "Person" shall mean any and all persons, natural or artificial, including any municipal, public or private corporation organized or existing under the laws of this or any other state or country, and any firm, partnership, or association of whatever nature.

2.4. "Owner/Operator" shall mean the person responsible for the compliance of the fuel burning units subject to the provisions of the Commission's Regulation II.

2.5. "Test Team Supervisor" shall mean the person, qualified by experience or education, who is charged with supervising the stack test. This person is responsible for ensuring the validity and correctness of the submitted test results.

2.6. "Laboratory Official" shall mean the person, qualified by experience or education, who is charged with overseeing or conducting the laboratory analysis of the collected samples. This person is responsible for ensuring the accuracy and validity of the laboratory results.

2.7. "Plant" shall mean and include all fuel burning units, source operations, equipment, and grounds utilized in an integral complex.

2.8. "Fuel Burning Unit" shall mean and include any furnace, boiler apparatus, device, mechanism, stack or structure used in the process of burning fuel or other combustible material for the primary purpose of producing heat or power by indirect heat transfer. For the purposes of this procedural rule, all fuel burning units are classified in the following categories:

a. Type 'a' shall mean any fuel burning unit which has as its primary purpose the generation of steam or other vapor to produce electric power for sale.

b. Type 'b' shall mean any fuel burning unit not classified as a Type 'a' or Type 'c' unit such as industrial pulverized fuel-fired furnaces, cyclone furnaces, gas-fired and liquid fuel-fired units.

c. Type 'c' shall mean any hand-fired or stoker-fired fuel burning unit not classified as a Type 'a' unit.

2.9. "Similar Units" shall mean all Type 'a', or all Type 'b', or all Type 'c' fuel burning units located at one plant.

2.10. "Fuel" shall mean any form of combustible matter (solid, liquid, vapor, or gas) that is used as a source of heat.

2.11. "Control Equipment" shall mean any equipment used for collecting or confining particulate matter for the purpose of preventing or reducing the emission of this air pollutant into the open air.

2.12. "Stack" shall mean, but not be limited to, any duct, control equipment exhaust, or similar apparatus, which vents gases and/or particulate matter into the open air.

2.13. "Particulate Matter" shall mean any material except uncombined water that exists in a finely divided form as a liquid or solid.

2.14. "Discharge Point" shall mean the point at which particulate matter is released from a stack into open air.

2.15. "Heat Input" shall mean the rate of heat release from all fuels fired in all similar units vented by the test stack during the test run period.

a. 'Design Heat Input (DHI)' shall mean the heat input level (in MM Btu/hr) for which an individual fuel burning unit has been designed to be operated during continuous operation.

b. 'Total Design Heat Inputs (TDHI)' shall mean the sum of the design heat inputs for all similar units located at one plant.

c. 'Normal Maximum Operating Load (NMOL)' shall mean the sum of the Design Heat Input levels (in MM Btu/hr) of the similar unit(s) vented by the test stack, unless the owner/operator has elected to operate one or more of the similar units vented by the test stack at or below a specified percentage of its Design Heat Input level as part of a compliance program, permit, or consent order officially accepted by the Commission. In such event, the NMOL shall be the sum of the Design Heat Input levels or fractions thereof as appropriate (i.e.,  $NMOL = 0.75 DHI_1 + DHI_2$ ).

2.16. "Normal Operation" when used in the context of fuel quality and combinations fired, shall mean the type, quality, and combination of fuel(s) fired which is representative of the fuel or fuel combination fired, in the unit(s) tested, over a reasonable period prior to the test, and the fuel or fuel combination which might reasonably be expected to continue to be fired in this unit after the test. If the type fuel, quality or combination used in the unit is variable, use the type, quality, and/or combination fired in day-to-day operation which can reasonably be expected to produce the greatest particulate matter loading to the control equipment (i.e., if coal is fired eight months out of the year and gas is fired four months out of the year, coal is to be burned during the test).

2.17. "ASTM" shall mean American Society for Testing and Material, 1916 Race Street, Philadelphia, Pennsylvania 19103.

2.18. "Sampling Plane" shall mean the imaginary plane located perpendicular to the gas flow in the duct or stack at the place selected for the extraction of the required samples.

2.19. "Probe" shall mean the part of the pitobe assembly (nozzle, sample tube, pitot tube, filter holder(s), sensor(s)), which precedes the last filter in the sampling

train and conveys the sample gas and particulate matter from the nozzle inlet to the last filter disc used for collecting stack particulate matter.

2.20. "Primary Filter" shall mean the last filter used in the sampling train to separate the particulate matter sample from the sampled stack gas.

2.21. "Prefilter" shall mean a filter used in the sampling train prior to the primary filter for the purpose of reducing the particulate matter build-up on the primary filter.

### Section 3. Symbols.

3.1.  $A_b = (S_d) \times (V_a)$ ,  $A_b$  is the estimate of the weight of residue, prior to use, in the acetone wash volume used (grams)

3.2.  $A_n =$  cross-sectional area of the sampling nozzle ( $ft^2$ )

3.3.  $A_s =$  cross-sectional area of the sampling plane ( $ft^2$ )

3.4. ASTM = American Society for Testing and Materials

3.5.  $B =$  percent moisture in the sampled gas, by volume, on a wet basis, divided by 100

3.6. BE = the boiler thermal efficiency (percent)

3.7. C = 453.592 grams/pound

3.8.  $^{\circ}C =$  degrees Centigrade

3.9. cfm = cubic feet per minute

3.10. CEM = continuous emission monitoring equipment

3.11. CO = carbon monoxide

3.12.  $CO_2 =$  carbon dioxide

3.13.  $d =$  diameter of nozzle (inches)

3.14. DGR = dry gas meter reading: the sample gas volume meter reading at meter conditions (cubic feet)

3.15.  $\Delta DGR =$  difference between two consecutive DGR's, the volume sampled at each sampling point (cubic feet)

- 3.16. EA = excess air fraction
- 3.17. F-factor = a factor representing a ratio of the dry flue gases generated to the calorific value of the fuel combusted (dscf/10<sup>6</sup> Btu)
- 3.18. Fi = quantity of each fuel fired in a fuel burning unit during the total test run period (in appropriate units)
- 3.19. °F = degrees Fahrenheit
- 3.20. Fp = combined correction factor for units and pitot tube deviation
- 3.21. ft<sup>3</sup> = cubic feet
- 3.22. ft/min = feet per minute
- 3.23. gm = grams
- 3.24. hbd = average enthalpy of steam/water leaving boiler as blowdown (Btu/lbm)
- 3.25. hi = average enthalpy of steam or other working fluid entering the boiler of the fuel burning unit (Btu/lb)
- 3.26. ho = average enthalpy of steam or other working fluid leaving the boiler of the fuel burning unit (Btu/lbm)
- 3.27. ΔH = pitot tube differential reading (inches H<sub>2</sub>O)
- 3.28. ΔHp = indicated differential pressure when the test pitot tube is used at the calibration point
- 3.29. ΔHs = indicated differential pressure when the standard pitot tube is used at the calibration point
- 3.30. Hg = mercury
- 3.31. HI = heat input per fuel burning unit(s) (10<sup>6</sup> Btu per hour)
- 3.32. H<sub>2</sub>S = hydrogen sulfide
- 3.33. HVf = higher heating value of the fuel on an as fired basis (in Btu/lbm)

3.34. HVi = average Btu value of each fuel used on an as fired basis, in appropriate units (Btu/lbm, Btu/gal, etc.)

3.35. in. Hg = inches of mercury, pressure

3.36. ISKo = overall isokinetic factor, ratio of total actual sample volume (Qm) to the total isokinetic sample volume (Qo), both volumes adjusted to standard conditions

3.37. ISKp = point isokinetic factor, ratio of the actual sample volume to the isokinetic sample volume

3.38. %ISK =  $100 (ISKo - 1)$

3.39. Kp = coefficient of deviation of the Type S pitot tube used in sampling, determined by calibration

3.40. Ks = coefficient of deviation for a standard pitot tube

3.41. lbf = pounds force

3.42. lbm = pounds mass

3.43. Ma = particulate matter obtained from the evaporation of the acetone washings (grams)

3.44. Mbd = average mass flow rate of blowdown (lbm/hr)

3.45. Mf = particulate matter collected by filter(s) (grams)

3.46. Mg = molecular weight of gas sample on wet basis

3.47. mf = average mass flow rate of steam through the boiler (lbm/hr)

3.48. mg = milligram

3.49. ml = milliliter

3.50. Mn =  $Mf + Ma - Ab$  (grams), indicated weight of particulate matter collected by the sampling train

3.51. n = number of items in a set of related items

3.52. N<sub>2</sub> = nitrogen

3.53. O<sub>2</sub> = oxygen

- 3.54.  $\Sigma$  = -- sum of all extraction times at all points sampled per run (min.)
- 3.55.  $P_b$  = -- atmospheric pressure (in. Hg)
- 3.56.  $P_f$  = . ash fraction of the non-metered fuel on an as fired basis
- 3.57.  $P_m$  = absolute pressure of gas at meter (in. Hg)
- 3.58.  $\overline{P_m}$  = average absolute pressure of the sampled gas at meter conditions for the test run (in. Hg)
- 3.59.  $P_s$  = absolute pressure of gas in stack at sampling plane
- 3.60.  $q_m$  = actual sample volume for each sample point adjusted to 68 °F and 29.92 in. Hg (ft<sup>3</sup>)
- 3.61.  $Q_m$  = sum of all  $q_m$  for each test run (ft<sup>3</sup>)
- 3.62.  $q_o$  = volume of sampled gas for each point if isokinetic conditions were maintained, adjusted to 68 °F and 29.92 in. Hg (ft<sup>3</sup>)
- 3.63.  $Q_o$  = sum of all  $q_o$  for each test run (ft<sup>3</sup>)
- 3.64.  $S_d$  = residue found in acetone blank (gm/ml)
- 3.65.  $\pi$  = -- pi, 3.1416
- 3.66.  $\Delta t$  = elapsed time at each sampling point (minutes)
- 3.67.  $T_f$  = temperature of the primary out-of-stack filter holder, when used (°F)
- 3.68.  $T_m$  = temperature of gas sample at volume meter for each point (°F)
- 3.69.  $\overline{T_m}$  = average temperature of gas sample at volume meter for test run (°F)
- 3.70.  $T_s$  = stack gas temperature (°F)
- 3.71.  $V_a$  = volume of acetone wash (ml)
- 3.72.  $V_{ac}$  = vacuum (inches of mercury)
- 3.73.  $V_m$  = sum of all  $\Delta DGR$  for the test run (ft<sup>3</sup>)
- 3.74.  $V_{mstd}$  =  $V_m$  corrected to standard conditions
- 3.75.  $w$  =  $1/(1 - B)$ , ratio of wet gas volume to dry gas volume

3.76. W =  $W_c + W_d$  (grams), amount of H<sub>2</sub>O removed from the sampled gas

3.77.  $W_c$  = amount of water collected in the condenser or impingers  
(grams)

3.78.  $W_d$  = amount of water collected by the drying agent in the absorber  
(grams)

3.79. % = percent

3.80. WVAPCC = West Virginia Air Pollution Control Commission

#### **Section 4. Adoption of Test Methods.**

4.1. For determining compliance with the mass emission rates as delineated in this Commission's Regulation II - "To Prevent and Control Particulate Air Pollution From Combustion of Fuel in Indirect Heat Exchangers", a person shall utilize those Reference Methods, in particular Method 5 or 17, as contained in 40 CFR, Part 60, Appendix A [as of July 1, 1988] with the following amendments:

a. Probe and filter media shall be maintained at, or about, stack temperature. In no case should temperature of probe or filter media exceed those of the stack.

b. Isokinetic conditions  $100\% \pm 10\%$  shall be maintained at each sampling point.

c. The result of each compliance test is to be the arithmetic average of three (3) complete sampling runs conducted within a seven (7) day period.

d. A complete sampling run shall be one complete determination of the total particulate matter emission rate through the test stack for which:

A. the minimum total sampling time is two (2) hours; and

B. the minimum total sample volume is sixty (60) cubic feet adjusted to 68 °F and 29.92 inches of Hg.

e. Any and all references in 40 CFR, Part 60, Appendix A, to the "Administrator" is amended to be the "Director".

In carrying out these methods for the purpose of determining mass emission rates, it is understood that other Reference Methods contained in 40 CFR, Part 60, Appendix A are integral parts of Methods 5 and 17 in particular, but not inclusive, Methods 1, 2, 3, and 4.

**Section 5. Unit Load and Fuel Quality Requirements.**

5.1. All compliance test runs, which are to be included in the test result for a unit or a specified number of units, shall be conducted while the unit or group of units is operated at or above the normal maximum operating load for the specified unit or group of units; while fuel or combinations of fuel representative of normal operation are being burned; and under such other relevant conditions as the Director may specify based on representative performance of the specified units.

**Section 6. Minor Exceptions.**

6.1. In the interest of practicality, the Director or his designee may allow minor exceptions, not related to test site safety, to the specifications of these methods, if the Director or his designee concludes that in a particular case, the granting of such exception would not invalidate the test results. If such exceptions are granted, alternate specifications may be prescribed.

6.2. If an exception as described above is granted, the scope of the exception and any alternative specification prescribed will be recorded in a letter of exception signed by the authorizing official. A copy of such letter of exception shall be attached to the test report.

**Section 7. Pretest and Post Test General Requirements.**

7.1. The owner/operator required to conduct tests and his test consultants must become familiar with the requirements of Regulation II - "To Prevent and Control Particulate Air Pollution From Combustion of Fuel in Indirect Heat Exchangers", Reference Methods as contained in 40 CFR, Part 60, Appendix A, and the requirements as delineated in this procedural rule, including all forms, equations, and definitions.

Questions of interpretation, applicability, or exception, must be resolved with the Director or his designee prior to conducting the test.

7.2. When a compliance test conducted in accordance with this procedural rule is required, the owner or operator of the affected unit(s) will be notified in writing by the Director or his designee. The notice will prescribe the following:

- a. the unit(s) to be tested;
- b. the identification number to be assigned to the test;
- c. the date by which the test is to be completed and the test report submitted; and

- d. the person, if other than the Director, to whom the test report is to be submitted, and with whom questions concerning the test procedure may be resolved. Test report forms (see Appendix) for filing the results of the compliance test are available from the Commission on request.

7.3. At least thirty (30) days prior to each compliance test, a test protocol must be furnished to the Director for his review and approval and must include as a minimum, the following information:

- a. Identification and description of the unit(s) that are to be tested.
- b. A discussion of the manner in which the unit(s) will be operated during the test periods with respect to operating loads, representativeness of fuel(s) fired, operating temperatures, and other factors which may affect emissions.

- c. A description or listing of unit and control equipment data that will be monitored and recorded during the test runs.

- d. A description of test methods and equipment that will be employed with requests for approval of any variances to test method procedures or sampling equipment designs set forth under these rules.

e. A drawing of the stack or duct sections where samples will be taken showing distances to upstream and downstream gas flow disturbances or bends and changes in duct or stack cross sections.

f. A drawing of the test plane(s) showing dimensions and number and location of sampling (traverse) points.

g. The sampling time at each traverse point and total sampling time for each test run. If the sampling time per traverse point is to be less than five (5) minutes, comments must be written concerning the variability of gas flow and temperatures during the shorter sampling time and how the sampling rate will be monitored and adjusted to maintain isokinetic conditions.

h. The minimum volume (SCF) of gas that will be sampled per test run.

i. Name of the person to contact concerning the scheduled tests and affiliation of personnel who will actually conduct the tests.

j. A copy of the last individual stack registration approved by the Director in accordance with Sub-section 3.1 (b) of the Commission's Regulation II.

k. A statement concerning where the laboratory analyses are to be conducted and description of chain of custody for collected samples.

7.4. Notification of the dates upon which compliance testing will be conducted must be provided to the Director, in writing, no later than fifteen (15) days prior to the date of the first test run so that he may, at his option, have an observer present during the test runs and sample analyses. Within constraints imposed by available facilities, copies of test field data sheets, laboratory sheets, unit operating logs and similar relevant data collected during the test runs shall be provided to the WVAPCC observer upon request at the conclusion of the tests. Any such data or other information so made available shall be treated as confidential upon request by the operator and shall not be made available to the public. The owner/operator shall place the word "confidential" upon all such information which is gathered and retained by the WVAPCC.

If facilities and circumstances allow, the WVAPCC test observer shall, at his option, observe the laboratory analyses.

7.5. A compliance test report providing the information summarized below and any additional information that the Director may require shall be submitted to the Director within sixty (60) days of the completion of the compliance testing.

a. General Information

- A. Plant name and location
- B. Units/stacks tested
- C. Name and address of company performing the tests
- D. Test dates and times

b. Report Certification

The following persons must certify that the test report contains true and accurate information:

- A. Test team supervisor
- B. Reviewer of test report (if applicable)
- C. If test is performed by source owner, the report must also

be certified by facility owner/operator

c. Test Summary

- A. Description of emissions sources/stacks tested
- B. Purpose of test
- C. Pollutants measured
- D. Operating data
  - (a) Unit(s) configuration and air pollution control equipment

flow diagrams.

(b) Summary of operating parameters including steam or electrical production rates and other relevant parameters measured and recorded and/or calculated for test periods should be attached to the report.

(c) Pertinent control equipment and operating data recorded and/or calculated for the test period should be attached to the report.

(d) Description of any unusual or non-typical operating mode, fuels, soot blowing, blowdown, etc. occurring or used during the tests.

d. Test Results

A. Mass emission test results with emissions reported in units of the applicable standard and in pounds per hour.

B. Visible emissions test results, if applicable, as measured by observer or transmissometer. If observed by personnel from test company or plant, evidence of observer's certification should be attached to the report.

C. Description of collected samples (if such information is deemed to be useful).

D. Description and discussion of real or apparent errors involved in test or process measurements, analysis, etc.

e. Test Procedures

A. Description of test equipment including drawing of sampling train.

B. Description of test procedures employed with detailed documentation of any deviations from methods required by this procedural rule.

C. Description of analytical procedures employed with detailed documentation of any deviations from methods required by this procedural rule.

D. Dimensioned drawing of sampling port location showing distances to upstream and downstream gas flow disturbances.

E. Cross-sectional drawing of sampling plane showing location and numbers or other designations of sampling points.

f. Appendix

A. Copies of original field data sheets from test runs.

B. Copies of original log sheets, strip charts and other process or control equipment data recorded during tests. These attachments should be certified by a responsible plant official.

C. Laboratory report including chain of custody.

D. Description of test equipment calibration procedures and calibration results for test equipment used.

E. Description of calibration performed on devices recording important operating data during the tests.

F. Copies of strip charts or other original outputs from continuous emission monitoring (CEM) equipment on the tested source and description of CEM system calibration and operation prior to and/or during tests.

G. Originals of any visible emission readings taken during test period.

H. Copies of relevant correspondence such as WVAPCC letters approving test method variances.

I. Names and titles of persons involved in the test including sampling team members, company personnel, and outside observers.

7.6. The result of each requested compliance test is to be the arithmetic average of three (3) complete sampling runs conducted, within one seven (7) day period, as prescribed by this procedure.

Subject to the provisions of Section 6 of this Rule, Minor Exceptions, a complete sampling run is one complete determination of the total particulate matter emission rate through the test stack for which:

- a. the minimum total sampling time is two (2) hours;
- b. the minimum sample time at each point is five (5) minutes.

c. the composite particulate matter sample is extracted from the duct or stack at a location and from the number of sampling points prescribed in Method 1 of 40 CFR, Part 60, Appendix A [as of July 1, 1988];

d. the sampling equipment and its method of operation for collection of particulate sample meets the criteria and requirements prescribed in Method 5 or Method 17 of 40 CFR, Part 60, Appendix A [as of July 1, 1988];

e. the overall sampling rate is within  $\pm 10\%$  of the overall isokinetic sampling rate, as calculated in Method 5 or Method 17 of 40 CFR, Part 60, Appendix A [as of July 1, 1988]; whichever is applicable and that the isokinetic ratio for each individual sampling point is within point  $\pm 10\%$  of the sample rate also;

f. the stack gas components data is determined as prescribed by Methods 3 and 4 of 40 CFR, Part 60, Appendix A, [as of July 1, 1988];

g. the other provisions of this procedural rule are met and sufficient heat input and fuel quality data is provided to verify that the requirements of Sub-section 7.6 h. below are met; and

h. sufficient data and commentary is provided with the submitted test report forms to allow the Director or his designee to evaluate the reported test results and the conditions under which they were obtained.

## **Section 8. Heat Input Data Measurements.**

### **8.1. General.**

a. The data measurements required to determine the total heat input to the fuel burning unit(s) vented by the test stack during the test run period depends on the computational method applicable.

This procedure prescribes three (3) computational methods:

Method 1H - Fuel Use Basis

Method 2H - Steam Balance Basis

Method 3H - Flue Gas Analysis Basis

The test supervisor is to submit data on the heat input(s) based on the Fuel Use Basis (Method 1H) whenever coal scales or other fuel meters, as appropriate, are available.

If the appropriate fuel metering device(s) are not available, Method 2H - Steam Balance Basis is to be used.

For all test runs also submit data on the heat input(s) based on Method 3H - Flue Gas Analysis Basis, in addition to the data required by Method 1H or 2H, whichever is applicable.

b. The following Sub-sections detail the specific data required for each method and the means of obtaining these data.

#### 8.2. Fuel Use Method (1H).

a. This computational method requires:

A. The measured amount of all fuel(s) fired in the fuel burning units during each test run period, as determined by continuous coal scales or equivalent and/or oil flow and/or gas meter(s). When gas is fired, the temperature and pressure of the gas meter(s) are needed.

B. The average moisture, ash, sulfur, volatile matter, and Btu value(s) of fuels fired in the fuel burning units during the test run period is to be determined and reported as follows:

(a) For coal:

(A) Obtain a representative sample of the coal fired in each fuel burning unit during the test run period. This sample is to be obtained in accordance with the Commercial Sampling Procedure of ASTM: Method D 2234-76 or its latest revision. Consult this ASTM standard for details of the required procedures.

(B) Prepare the reduced gross sample, obtained above, for laboratory analysis in accordance with ASTM: Method D 2013-72, "Preparing Coal Samples for Analysis" or its later revision. Consult this ASTM standard for details

of the required procedure. In this ASTM method, further amplification is given to the methods of reducing the gross sample to a laboratory sample and preparing the laboratory analysis. The laboratory sample is so prepared that 100% of the coal sample will pass through a No. 60 (250 micron) sieve. The final product is thoroughly mixed prior to extracting analytical samples.

(C) Extract an analytical sample from the laboratory sample and determine the moisture, ash, and volatile matter content of this sample in accordance with ASTM: Method D 3173-73 (Moisture), ASTM D 3174-73 (Ash), and ASTM D 3175-73 (Volatile Matter). Consult these ASTM standards for details of the required procedures. In these ASTM methods, procedures are prescribed for determining the moisture, ash, and volatile content of the sample.

(D) Extract another analytical sample from the laboratory sample and determine the Btu content of the sample in accordance with ASTM: Method D 2015-77 "Gross Calorific Value of Solid Fuel by the Adiabatic Bomb Calorimeter" or its latest revision. Consult this ASTM standard for details of the required procedure.

(E) Extract another analytical sample from the laboratory sample and determine total sulfur content of the sample in accordance with ASTM: Method D 3177-75 "Test for Total Sulfur in the Analysis Sample of Coal and Coke" or its latest revision. Consult this ASTM standard for details of the required procedures.

(F) Send a sealed and marked one pint sample of the laboratory sample representative of the gross sample, to the Commission with the test report. If drying was used in reducing the gross sample to the laboratory sample, indicate the percent loss of moisture during this process. For each container provide the test identification number assigned by the WVAPCC in accordance with Sub-section 7.2 of this rule and the test run number.

(b) For Fuel Oils:

Determine the supplier's name and address, and the specifications for the oil supplied. Use the supplier's specifications when available for the ash content and Btu value of the oil. When such specifications are not available, determine the grade of oil fired, by referring to any Standard Engineering Handbook. As such the Handbook and appropriate edition should be properly identified, for inclusion as part of any results submitted to the agency for the ash, sulfur and Btu values. Send an eight ounce, sealed and marked, sample of the oil fired during the test to the Commission with the test report.

(c) For Natural Gas:

Determine the supplier's name and address, and the specification of the natural gas supplied. Use the supplier's specification for the Btu value of the fuel. Ash may be considered negligible.

(d) Other Fuels:

Determine the name and address of the supplier(s) or producer(s) of any other materials fired during the test run period. Determine the source(s) of the fuel(s). Use the supplier(s)/producer(s)' specifications for the ash, sulfur, and Btu value. When such specifications are not available, resolve with the Director or his designee, the method which will be used to determine these values, prior to conducting the test. Submit an appropriate small sample of the fuel fired, if other than a gas, to the Commission in a sealed and marked sample container.

8.3. Steam Balance Method (2H).

This method requires a materials balance and inlet and outlet water/steam or other media pressure and temperature data during the test run period, for the boiler(s) of the fuel burning unit(s) vented by the test stack.

a. Measure the mass flow rate of all water/steam or other media flowing through each boiler, including blowdown.

b. Measure the inlet and outlet pressure and temperature of each water/steam circuit, including blowdown.

c. Construct a flow diagram of the water/steam or other media flow circuit(s) on Form THI-II (2H). Record the measured data on this form, indicating the data points on the diagram.

d. Determine the boiler manufacturer's name and address, and the boiler type and model number. From the manufacturer's specification, determine the boiler(s) thermal efficiencies. If such specifications are not available, describe in detail the basis and method of selecting the value used.

#### 8.4. Flue Gas Analysis Method (3H).

a. This method involves determining the heat input for the boiler(s) of the fuel burning unit(s) vented by the test stack utilizing:

A. Appropriate F-factors as contained in 40 CFR, Part 60, Subpart D [as of July 1, 1988]; and

B. Total volume of stack gas discharged through the stack during the test run; and

C. The average excess air discharged [O<sub>2</sub>% or CO<sub>2</sub>%] through the test stack during the test run period.

b. Appropriate F-factors are to be obtained from 40 CFR, Part 60, Subpart D [as of July 1, 1988], unless carbon content of fly ash or bottom ash exceeds five (5) percent on a per weight basis. In these cases, consult the Director or his designee prior to conducting the test to determine and resolve a suitable F-factor adjustment.

c. Total Volume of Stack Gas.

The total volume of stack gas is determined from:

A. Volume meter readings obtained during subject test run and recorded on Form TD: Test Run Data Sheet for each test run.

d. Stack Excess Air.

A. For low nitrogen content fuel(s) (coal, fuel oil, natural gas), the stack excess air can be computed from the data obtained from the Orsat analysis and recorded on Form TOA - Laboratory Data Sheet (Orsat) for each test run. If blast furnace gas, producer gas, or other fuel(s) of high nitrogen content are used, consult the Director or his designee prior to conducting the test to determine and resolve a suitable method of determining the excess air when such fuel(s) is burned.

**Section 9. Computations and Data Analysis.**

This section prescribes the computational method to be used in computing the particulate matter stack emission rate for the test and evaluating the supporting test data. Perform the computations and analysis prescribed in this section for the data obtained from each test run which is to be part of the submitted test results. Record the measured data and the appropriate computations on the designated test report forms, a copy of which is in the Appendix. Submit sufficient commentary with the test report data to fully describe the conditions under which the data was obtained and any factors which might affect the evaluation of the test results.

9.1. Particulate Matter Sample Weight Determination. (Form TLP - Laboratory Data Sheet (Particulate)).

$M_f$  = particulate matter (grams) collected by the primary filter, including any prefilter if used

$M_a$  = particulate matter (grams) obtained from the evaporation of the acetone washings of the internal sampling train surfaces exposed to the particulate sample prior to the primary filter

$A_b$  = particulate matter residue (grams) in the volume ( $V_a$ ) of acetone wash used for  $M_a$  above, as determined by the acetone blank analysis [i.e.,  $A_b = (S_d)(V_a)$ ; where  $S_d$  equals the residue found in the acetone blank analysis in gm/ml, and  $V_a$  equals the volume of acetone used in the acetone wash for  $M_a$  above]

$M_n = M_f + M_a - A_b =$  the indicated weight of particulate matter collected, in grams

9.2. Moisture Determination. (Form TLH: Laboratory Data Sheet - Moisture; Forms TD; Test Run Data Sheet).

Record all measured and calculated data on the appropriate forms. Compute and record the following:

$V_m =$  (ft<sup>3</sup>) the sum of all  $\Delta$  DGR for the run, where  $\Delta$  DGR is equal to the indicated amount of gas sampled at each point during the extraction interval

$\bar{T}_m =$  (°F) average temperature of the dry gas meter during the test run.  $T_m =$  average dry gas meter temperatures (°F) at each sampling point.

$\bar{P}_m =$  (in. Hg) average absolute pressure at the dry gas meter during the test run.  $P_m =$  the average absolute pressure at the dry gas meter for each sample point, where  $P_m = P_b - V_{ac}$ ;  $P_b =$  barometric pressure,  $V_{ac} =$  meter vacuum.

$W_c =$  amount of water collected in condenser or impingers (grams)

$W_d =$  amount of water collected by the drying agent used after the condenser or impingers (grams)

$W = W_c + W_d$  (grams)

$B =$  percent moisture in the sampled gas by volume on a wet basis, divided by 100

$$B = W / \left[ \frac{374 \bar{P}_m V_m}{\bar{T}_m + 460} + W \right]$$

$w =$  moisture correction factor; ratio of the volume of wet sample gas to the volume of dry sample gas

$$w = 1 / (1 - B)$$

9.3. Sample Gas Density and Excess Air Determination. (Form TOA - Laboratory Data Sheet (Orsat)).

a. Gas Density.

A. Record the Orsat analysis for all three runs on Form TOA (Laboratory Data Sheet) on lines 1 through 9. Compute and record the average value of  $\text{CO}_2$ ,  $\text{O}_2$ ,  $\text{CO}$  and  $\text{N}_2$  for each run on line 10 or the value of these components of the composite sample, if obtained (optional), on line 11.

B. Transcribe the values of  $w$  (moisture correction factor) from Form TLH to Form TOA in blocks 12 for each run. Transcribe the values of  $B$ , the percent water (wet basis) from Form TLH to Form TOA in column 13, line 14, for each run.

C. Correct the average component volumetric percentages, dry basis (line 10), to volumetric fractions (wet basis), by dividing by  $100w$  and enter these values on line 14 for each test run.

D. Multiply each of these volumetric fractions (wet basis - line 14) by the corresponding molecular weights on line 15 and enter the values on line 16.

E. Enter the sum of the values on line 16 for each run in the appropriate box on line 17, the apparent molecular weight of the wet gas ( $M_g$ ).

F. -- Determine the wet gas density for each run by dividing the molecular weight for the run (on line 17) by the number 29 and enter this quotient in the appropriate box on line 18.

b. Excess Air.

Compute and record the excess air fraction for each run using the average dry gas analysis from line 10 and the formula shown on line 20. Record the excess air fraction (EA) in the appropriate box on line 19.

Note: The excess air fraction equation presented on line 20 of Form TOA is not applicable when producer gas, blast furnace gas or other fuels high in nitrogen content are used.

9.4. Actual Sample Gas Volume Determination. (Form TD: Test Run Data Sheet).

a. For each point sampled during the run compute the actual volume drawn through the sampling nozzle adjusted to standard conditions of 68 °F and 29.92 inches of Hg as indicated below:

$q_m$  = Actual sample volume (in cubic feet) drawn through the sampling nozzle for each sampled point adjusted to 68 °F and 29.92 inches of Hg.

$$q_m = (\Delta DGR) (w) \cdot \frac{528}{(T_m + 460)} \cdot \frac{P_m}{29.92}$$

WHERE,

$\Delta DGR$ ,  $w$ ,  $T_m$ , and  $P_m$  are defined in Sub-section 9.2 of this section and are recorded on Form TD.

b. Record the computed values of  $q_m$  for each sampled point on the appropriate line of the column labeled  $q_m$  on Form TD. Sum the values of  $q_m$  for all points included in the run and enter this value ( $Q_m$ ) in the block so labeled.

9.5. Isokinetic Sample Volume Determination. (Form TD: Test Run Data Sheet).

a. For each point sampled during the run, compute the volume of sample gas (adjusted to 68 °F and 29.92 inches of Hg) that would have been drawn through the sampling nozzle if isokinetic conditions were maintained, as indicated below:

$q_0$  = Isokinetic sample volume, the volume of sampled gas (in cubic feet) for each sampled point, if isokinetic conditions were maintained, adjusted to standard conditions of 68 °F and 29.92 inches of Hg. For conditions where static pressure in the duct or stack being tested is more than 20 in. H<sub>2</sub>O, consult with Director or his designee.

$$q_0 = 60 (528) (F_p) (A_n) \cdot \left[ \frac{\Delta H}{T_s + 460} \right]^{.5} \cdot \Delta t$$

WHERE,

$F_p$  = combined correction factor for units and Pitot tube deviation:

$$\text{Standard tube} = 2.90 \text{ (units)} \times 1.00 \text{ (deviation)} = 2.90$$

Type S tube = 2.90 (units) x 0.83\*(deviation) = 2.41

\*Note: The deviation for the Type S tube may vary for different sampling configurations and should be determined by calibration against a standard pitot tube for each Pitobe arrangement per Method 2 of 40 CFR, Part 60, Appendix A [as of July 1, 1988].

$A_n$  = the cross-sectional area of the sampling nozzle in (ft<sup>2</sup>)

$\Delta H$  = Pitot tube differential reading\*\* in inches of H<sub>2</sub>O

\*\*Note: If the particular pitot tube differential indicator used is calibrated to give a reading of the square root of  $\Delta H$  ( $\sqrt{\Delta H}$ ), change the heading of the " $\Delta H$ " column on Form TD to  $\sqrt{\Delta H}$  and modify your computations for  $q_0$  as appropriate.

$T_s$  = Average stack gas temperature (in °F) at each sampled point during the extraction time at that point.

$\Delta t$  = elapsed time at each sampling point (minutes)

b. Record the computed values of  $q_0$  for each sampled point on the appropriate line of the column labeled  $q_0$  on Form TD. Sum the values of  $q_0$  for all points included in the run and enter this value ( $Q_0$ ) in the block so designated.

#### 9.6. Fractional Isokinetic Rate Determination. (Form TD: Test Run Data Sheet).

a. For each point sampled during the run, compute the point isokinetic factor (ISK<sub>p</sub>), which indicates the average degree of deviation from isokinetic conditions during the sampling (extraction) time at that point. ISK<sub>p</sub> is computed as follows:

ISK<sub>p</sub> = the point isokinetic factor, the ratio of the actual sample volume to the isokinetic sample volume, both volumes adjusted to standard conditions of 68 °F and 29.92 inches of Hg

$$ISK_p = \left[ \begin{array}{c} q_m \\ \hline q_o \end{array} \right]$$

WHERE,

$q_m$  is defined in Sub-section 9.4 and  $q_o$  is defined in Sub-section 9.5 of this part, both values are recorded for each point on Form TD.

b. Record the computed values of  $ISK_p$  for each sampled point on the appropriate line of the column labeled  $ISK_p$  on Form TD. The value of  $ISK_p$  for each sampled point should not vary greatly from the overall isokinetic factor for the run  $ISK_o$ .

c. For each run, compute the overall isokinetic factor ( $ISK_o$ ), which indicates the overall degree of deviation from isokinetic conditions during the run, and which is used in the weight emission rate computations of the next section.  $ISK_o$  is computed as follows:

$ISK_o$  = the overall isokinetic factor, the ratio of the total actual sample volume to the total isokinetic sample volume, both volumes adjusted to standard conditions of 68 °F and 29.92 inches of Hg.

$$ISK_o = \left[ \frac{Q_m}{Q_o} \right]$$

WHERE,

$Q_m$  is defined in Sub-section 9.4 and  $Q_o$  is defined in Sub-section 9.5, both values are recorded for each run on Form TD.

d. Record the computed value of  $ISK_o$  for each run in the block so designated on Form TD. If the value of  $ISK_o$  is outside the range of 0.9 to 1.10, reject the run result.

e. Compute the value %ISK as follows: retain the sign and record on Form TR-II: Summary of Test Run Results.

$$\%ISK = 100 \left[ ISK_o - 1 \right]$$

9.7. Particulate Matter Emission Rate Determination. (Form TD: Test Run Data Sheet, Form TR-II: Summary of Test Run Results).

The particulate matter emission rate for each run is computed from the following equation:

$$M(P)n = \frac{Mn}{C} \cdot \frac{As}{An} \cdot \frac{60}{\ominus} \cdot \frac{1}{ISKo}$$

WHERE,

$M(P)n$  = the particulate matter emission rate (in pounds per hour) for the test run

$Mn$  =  $Mf + Ma - Ab$  indicated weight of particulate matter (in grams) collected by the sampling train.

$C$  = 453.592 grams/pound

$As$  = the cross-sectional area of the sampling plane (ft<sup>2</sup>)

$An$  = the cross-sectional area of the sampling nozzle (ft<sup>2</sup>)

60 = 60 minutes per hour

$\ominus$  = the sum of all extraction times at all points sampled per run (the sum of  $\Delta t$ 's). The total sampling time, not including movement time from port to port.

$ISKo$  =  $Qm/Qo$  = the overall isokinetic factor for the run. The ratio of total actual volume sampled to the total isokinetic volume, both values adjusted to 68 °F and 29.92 inches of Hg on a wet basis.

The values of  $Mn$ ,  $As$ ,  $An$ ,  $\ominus$ , and  $ISKo$  for each run are recorded on Form TD: Test Run Data Sheet.

Record the value of  $M(P)n$  for each test run on Form TR-II: Summary of Test Run Results.

9.8. If more than one sampling plane was required to evaluate the total stack emission rate, perform the computation specified in 9.7 for each sampling plane, then sum the values of  $M(P)n$  for all sampling planes used. Record the total emission rate

for each run (all sampling planes) on Form TR-II as above, then compute the average stack emission rate for the test. Note the number and designations of the sampling planes used under comments. If more than one sampling train was used simultaneously to sample the required number of sampling points at one sampling plane, the values of Mn, Qm, and Qo are the sum total values for all the sampling trains used for the one sampling plane.

9.9. Heat Input Determinations.

(Forms THI-II: Heat Input Data Sheets: Form TOA; Laboratory Data Sheet (Orsat); Form TR-II: Summary of Test Run Results).

a. This Sub-section prescribes three (3) methods of computing the total heat input to the (similar) fuel burning unit(s) vented by the test stack:

Method 1H - Fuel Use Basis

Method 2H - Steam Balance Basis

Method 3H - Flue Gas Analysis Basis

Submit data and computations on the appropriate forms.

b. Summarize the results of the selected computational methods on Form TR-II: Summary of Test Run Results for each run. Record the type units tested (see definitions for type), the total number of similar units associated with the test run results, the two values of the total heat input for all the units associated with the test run results, as computed by the two selected methods, the total design heat input and the total maximum normal operating load for the units associated with the test result (see definitions for the heat input terms).

9.10. Method 1H - Fuel Use Basis.

a. From the data obtained in accordance with Sub-section 8.2, Heat Input Data Measurements, compute the heat input for each fuel burning unit for which this method is to be used, as follows:

$$HI = \frac{60}{\Theta} \sum_{i=1}^n \frac{(F_i \times HVi)}{10^6}$$

WHERE,

HI = Heat input per fuel burning unit(s) in  $10^6$  Btu per hour

$F_i$  = The quantity of each fuel fired in this fuel burning unit during the total test run period ( $\Theta$ ) in appropriate dimension units (e.g., pounds, gallons, SMCF)

$HVi$  = The average Btu value of each fuel used, in appropriate dimensional units related to the  $F_i$  units (e.g., Btu/lb, Btu/gal, Btu/SMCF), on an as fired basis

$\Theta$  = The total test run period in minutes. The sum of all extraction intervals ( $\Delta t$ )

$n$  = The number of different fuels fired in the fuel burning unit during the test run period

NOTE: When more than one fuel burning unit is vented by the test stack, sum the individual heat input values for all units of the same type vented by the test stack to obtain the total heat input for the test.

b. Record the values used in the computations, and the results on Form THI-II (1H)

9.11. Method 2H - Steam Balance Basis.

a. From the data obtained in accordance with Sub-section 8.3, compute the heat input for each fuel burning unit for which this method is to be used, as follows:

$$HI = \frac{mf (ho - hi) + Mbd (hbd)}{10^4 (BE)}$$

WHERE,

HI = Heat input per fuel burning unit in  $10^6$  Btu per hour

ho = Average enthalpy of steam/water or other media leaving the boiler of the fuel burning unit in Btu/lbm

hi = Average enthalpy of steam/water or other media entering the boiler of the fuel burning unit in Btu/lb

mf = Average mass flow rate of steam/water or other media through the boiler in lbm/hour

Mbd = Average mass flow rate of blowdown in lbm/hour

hbd = Average enthalpy of steam/water or other media leaving boiler as blowdown in Btu/lbm

BE = The boiler thermal efficiency (percent)

NOTE: The enthalpy values for the above equation can be determined from the inlet and outlet temperatures and pressures of the steam/water or other media flowing through the boiler using appropriate steam tables.

b. Record the steam flow, temperatures, pressures, and enthalpy values on the steam/water or other media circuit flow diagram required on Form THI-II (2H). Also record the necessary calculations and results on Form THI-II (2H) or attached sheet(s). Sum the heat input values of all fuel burning units of the same type vented by the test stack.

9.12. Method 3H - Flue Gas Analysis Basis:

a. From data obtained in accordance with Sub-section 8.4, compute the heat input for each fuel burning unit for which this method is to be used, as follows:

$$HI = \frac{Vmstd \cdot \frac{As}{An} \cdot \frac{20.9 - \%O_2}{20.9}}{F\text{-factor} \cdot \frac{\ominus}{60}}$$

WHERE,

HI = Heat input per fuel burning unit in 10<sup>6</sup> Btu per hour

Vmstd = Volume of gas sample measured by the dry gas meter during run corrected to standard conditions of 68 °F and 29.92 inches Hg.

As = Cross-sectional area of the sampling plane (ft<sup>2</sup>)

An = Cross-sectional area of the sampling nozzle (ft<sup>2</sup>)

%O<sub>2</sub> = Percent oxygen content by volume as taken from Orsat analysis on Form TOA

F-factor = a factor representing a ratio of the dry flue gases generated to the calorific value of the fuel combusted (dscf/10<sup>6</sup> Btu), See 40 CFR, Part 60, Subpart D

⊖ = Sum of all extraction time at all points sampled per run (minutes)

b. Record Vmstd, %O<sub>2</sub>, F-factor, and ⊖ on Form THI-II (3H). Record calculations.

**Section 10. Inconsistency Between Regulations.**

10.1. In the event of any inconsistency between this regulation and any other regulation of the Commission, such inconsistency shall be resolved by the determination of the Director and such determination shall be based upon the application of the more stringent provision, term, condition, method, rule or regulation.

The foregoing is a true and correct copy of the West Virginia Air Pollution Control Commission Regulation TP-2.

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Carl G. Beard, II  
Secretary  
West Virginia Air Pollution  
Control Commission

# STACK TEST REPORT

Facility \_\_\_\_\_

Unit(s) \_\_\_\_\_

Stack \_\_\_\_\_

Conducted by

\_\_\_\_\_

Under Regulation \_\_\_\_\_

Submitted on \_\_\_\_\_

to the

STATE OF WEST VIRGINIA

AIR POLLUTION CONTROL COMMISSION

Subject: STACK TEST REPORT

TEST NUMBER

[Empty box for Test Number]

To:

West Virginia Air Pollution Control Commission  
1558 Washington Street, East  
Charleston, WV 25311

(For WVAPCC Use Only)

IDENTIFICATION

1. Facility

A. Parent Organization \_\_\_\_\_

B. Facility Name \_\_\_\_\_

C. Facility Address/Location \_\_\_\_\_  
\_\_\_\_\_

D. Individual to Contact Regarding this Report:

Name \_\_\_\_\_

Title \_\_\_\_\_

Address \_\_\_\_\_

Telephone \_\_\_\_\_

E. Source Operation Tested \_\_\_\_\_  
\_\_\_\_\_

F. Type of Control Equipment \_\_\_\_\_  
\_\_\_\_\_

G. Stack Designation \_\_\_\_\_

TEST SUPERVISOR (type)	(Signature)	(Date)



SAMPLING SITE DATA SHEET	Site Identification #		
Sampling Plane Schematic: (Show cross-sectional dimensions, port and point locations, deposit buildup, etc.)	Point Sampling time ( $\Delta t$ ):		
	(1) As:	ft <sup>2</sup>	
	(2) Nearest Upstream Disturbance	Dia's	
	(3) Nearest Downstream Disturbance		
	(4) For Rect. Ducts: Equal Areas	l/w ratio	
	Minimum Required No. of Points		
Diameter or Equivalent Diameter*:	By Item	No. Points	Ck
Sampling Site Layout. (Show dimensions, general arrangement, bends, baffles, disturbances, with respect to the sampling plane.)			
*Eq Dia = $2 \sqrt{(\text{length})(\text{width})/(\text{length} + \text{width})}$ ; for Rectangular Ducts.			

Continuation:





LABORATORY DATA SHEET  
(Particulate)

Test #:

ITEM/IDENTIFICATION

WEIGHT (GRAMS)

(1) Prefilter

Run #1      Run #2      Run #3

R1 R2 R3 B

IDN     (1)


(2) Primary Filter

Run #1      Run #2      Run #3

R1 R2 R3 B

IDN     (2)


Mf = sum of (1) & (2)

(3) Acetone Wash

Run #1      Run #2      Run #3

R1 R2 R3 B

IDN     Ma

Sd = (a)/(b)      Va =

Sd =  gm/ml

Ab = (Va)(Sd) =


Blank(s)

	After
	Tare
(a)	Change
(b)	Wash Volume (ml)

Summation

Prefilter = (1) =

Primary Filter = (2) =

Acetone Wash Ma =

Subtotal =

-Ab =

Mn =


Laboratory Official (type)

(Signature)

(Date)

Stack Test Report

LABORATORY DATA SHEET (Moisture)	Test #
-------------------------------------	--------

ITEMS/IDENTIFICATION	WEIGHT(gms)/VOLUME*(ml)						
	Run #1	Run #2	Run #3				
(1) Impingers/Condensers  IDN <u>  R1  </u> <u>  R2  </u> <u>  R3  </u> <table border="1" style="display: inline-table; border-collapse: collapse; margin-left: 10px;"> <tr> <td style="width: 30px; height: 20px;"></td> <td style="width: 30px; height: 20px;"></td> <td style="width: 30px; height: 20px;"></td> </tr> </table> Wc=				<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	after tare change
(2) Desiccant Containers  IDN <u>  R1  </u> <u>  R2  </u> <u>  R3  </u> <table border="1" style="display: inline-table; border-collapse: collapse; margin-left: 10px;"> <tr> <td style="width: 30px; height: 20px;"></td> <td style="width: 30px; height: 20px;"></td> <td style="width: 30px; height: 20px;"></td> </tr> </table> Wd=				<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	after tare change
(3) Summation:    W=Wc + Wd =	<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	<table border="1" style="width:100%; height: 20px;"></table>	TOTAL GRAMS			

(4)  $B = W / [ \{ 374 (\overline{Pm}) (Vm) / (\overline{Tm} + 460) \} + W]$

Run #1:    B = (        ) / [ { 374 (        ) (        ) / (        ) } + (        ) ] =

Run #2:    B = (        ) / [ { 374 (        ) (        ) / (        ) } + (        ) ] =

Run #3:    B = (        ) / [ { 374 (        ) (        ) / (        ) } + (        ) ] =

(5)  $w = 1/(1-B)$

w = moisture correction =

Run #1	Run #2	Run #3

factor

\*1 ml equivalent to 1 gram to room temperature

LABORATORY OFFICIAL (type)	(Signature)	(Date)
----------------------------	-------------	--------

Stack Test Report

LABORATORY DATA SHEET  
(Orsat)

Test #

Run #1					Run #2					Run #3				
Date					Date					Date				
% By Vol., (Dry Basis)					% By Vol., (Dry Basis)					% By Vol., (Dry Basis)				
Time	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>	Time	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>	Time	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>
1														
2														
3														
4														
5														
6														
7														
8														
9														
10	Avg				Avg					Avg				
11	Comp				Comp					Comp				

12 w =  (13)  
% by vol. (Wet Basis)(B)      w =  (13)  
% by vol. (Wet Basis)(B)      w =  (13)  
% by vol. (Wet Basis)(B)

	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>	H <sub>2</sub> O	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>	H <sub>2</sub> O	CO <sub>2</sub>	O <sub>2</sub>	CO	N <sub>2</sub>	H <sub>2</sub> O
14															
15	44	32	28	28	18	44	32	28	28	18	44	32	28	28	18
16															

17 Mol Wt =  =Mg       =Mg       =Mg

18 Mg/29 =  =      Mg/29 =  =      Mg/29 =  =

19 Ex. Air =  = EA      Ex. Air =  =EA      Ex. Air =  = EA

20 WHERE EA\* = 
$$\frac{(\%O_2) - (\%CO/2)}{0.264 (\%N_2) - (\% O_2) + (\%CO/2)}$$

\*Not applicable when procedure gas, blast furnace gas, or other fuels high in N2 are used.

LABORATORY OFFICIAL (Type)      (Signature)      (Date)

Stack Test Report  
 LABORATORY DATA SHEET  
 (Fuels)

TEST #

Sample Number	Fuel Sampling Data			Type Fuel	Fuel Quality Data				Prior* Surface Moisture lost (%)
	Gross* Sample lbs	Increments (No.)	Laboratory* Sample lbs		Moisture as rec'd % by Wt.	Ash as rec'd % by Wt.	Sulfur as rec'd % by Wt.	Btu Content as rec'd Btu/lb	
Run #									
Run #									
Run #									
TEST SUPERVISOR (type)			LABORATORY OFFICIAL (type)						
(Signature)			(Signature)						
* Note surface moisture lost during reduction of gross coal sample to laboratory sample in percent (%), as applicable.									





HEAT INPUT DATA SHEET - 2H  
(Steam Balance Basis)

Run #

Continuation:

$$HI = \frac{Vmstd \cdot \left[ \frac{As}{An} \right] \cdot \left[ \frac{20.9 - \%O_2}{20.9} \right]}{10^6 \cdot [F\text{-factor}] \cdot 1/60 \cdot \theta}$$

WHERE,

$$\frac{As}{An} =$$

F-factor =

Run #	Vmstd (dscf)	%O <sub>2</sub>	θ (minutes)	HI (10 <sup>6</sup> Btu/hr)